A Staggered Grid Numerical Method for the Navier-Stokes Equation

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Abstract— We consider incompressible fluid flows governed by the two-dimensional Navier-Stokes equation. The Navier-Stokes equation is solved numerically using a staggered grid finite difference method. Our aim in this paper is to assess the performance of this numerical method for the Navier-Stokes equation. The lid-driven cavity problem is taken into account to test the numerical method. In order to achieve our aim we focus on the motion of the fluid, and in particular, its velocity. Our results are compared with some available benchmark data.

Keywords – finite difference method, lid-driven cavity flow, Navier-Stokes equation, staggered grid.

1 INTRODUCTION

The Navier-Stokes equation has been used to simulate both compressible and incompressible fluid flows. Its analytical solution is not available in general, until this paper is written. Due to its wide applications, a robust numerical method is desired. Some simplification of the Navier-Stokes equation are also available, such as the Euler equation for gas dynamics and the Saint-Venant system for shallow water flows. This paper deals with incompressible fluid flows governed by the two-dimensional Navier-Stokes equation.

A number of authors (see for example [1]-[6]) attempted to solve the Navier-Stokes equation. Biringen and Chow [1] provides a detailed explanation on several staggered grid finite difference methods. Harlow and Welch [2] proposed a staggered grid method called the Marker-And-Cell. Huser and Biringen [3] solved the Navier-Stokes equation using a staggered grid method modified from some other authors. Li [4] proposed an adaptive grid method, where grid positions with large errors are refined. Erturk et al. [5] provides benchmark data that can be used to assess a new numerical method for the Navier-Stokes equation. Moin et al. [6] proposed necessary conditions for the stability of staggered grid methods.

In this paper we are interested in assessing the staggered grid finite difference method presented by Biringen and Chow[1]. We compare the numerical results with available benchmark data of Erturk et al. [5]. The comparison gives idea about difficulty, accuracy and robustness of the the staggered grid finite difference method. This kind of comparison was not given in the work of Biringen and Chow[1]. Therefore, this paper completes the work of Biringen and Chow[1].

The rest of this paper is organized as follows. The Navier-Stokes equation is recalled in Section 2. The staggered grid finite difference method is summarized in Section 3. Numerical results of this staggered grid method are presented and compared with benchmark data in Section 4. Finally, Section 5 draws some concluding remarks.

2 THE NAVIER-STOKES EQUATION

In this subsection we recall the Navier-Stokes equation in two dimensions [1]. It is given by the following system:

$\nabla . \mathbf{V} = 0,$		(1)

$$\frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{V} = -\overline{V}P + \mathrm{Re}^{-1} \nabla^2 \mathbf{V}.$$
(2)

Here, the quantities are dimensionless. The free variables are time *t* and space (x, y). The vector $\mathbf{V} = [u \ v]^T$ where u = u(x, y, t) is the velocity at the *x*-direction and v = v(x, y, t) is the velocity at the *y*-direction. The variable $P = p / \rho$, where is thermodynamic pressure and ρ is the fluid density. Using (1) we define

$$\mathbf{H} = \mathbf{V} \cdot \nabla \mathbf{V} = \nabla \mathbf{V} \cdot (\mathbf{V}\mathbf{V}). \tag{3}$$

The Reynolds number Re is defined as

$$\operatorname{Re} = \frac{U_o L}{\mu},\tag{4}$$

in which U_o is the characteristic velocity scale, L is the characteristic length and μ is the viscosity of the fluid. Note that

$$\mathbf{V} \cdot \nabla \mathbf{V} = \nabla (\mathbf{V}\mathbf{V}) - \mathbf{V}\nabla \cdot \mathbf{V}. \tag{5}$$

Employing the continuity (1), we have

$$\mathbf{V}\nabla\cdot\mathbf{V}=\mathbf{0}.$$

Therefore, we obtain

$$\mathbf{V} \cdot \nabla \mathbf{V} = \begin{pmatrix} \frac{\partial u^2}{\partial x} + \frac{\partial uv}{\partial y} \\ \\ \frac{\partial uv}{\partial x} + \frac{\partial u^2}{\partial y} \end{pmatrix}.$$
 (7)

The the Navier-Stokes equation can now be rewritten as

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 , \qquad (8)$$

$$\frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uv}{\partial y} = \operatorname{Re}^{-1} \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) - \frac{\partial P}{\partial x}, \qquad (9)$$

$$\frac{\partial v}{\partial t} + \frac{\partial uv}{\partial x} + \frac{\partial v^2}{\partial y} = \operatorname{Re}^{-1} \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - \frac{\partial P}{\partial y} \,. \tag{10}$$

Here (8) is equivalent to (1). Equations (9) and (10) are equivalent to (2).

3 THE NUMERICAL METHOD

In this section, we summarize the staggered finite difference method that was used by Biringen and Chow [1]. The predictor-corrector finite difference method is applied. First we consider the evolution from time t^n to \hat{t} . When the pressure gradient is omitted, the Crank-Nicolson scheme is used to discretize the time and the Adams-Bashforth is used to discretize the convective terms, we have

$$\frac{\hat{\mathbf{V}} - \mathbf{V}^n}{\Delta t} = -\frac{3}{2}\mathbf{H}^n + \frac{1}{2}\mathbf{H}^{n-1} + \frac{1}{2\operatorname{Re}}\nabla^2(\hat{\mathbf{V}} + \mathbf{V}^n).$$
(11)

Then in the similar way, the evolution from time t^n to t^{n+1} leads to

$$\frac{\mathbf{V}^{n+1} - \mathbf{V}^n}{\Delta t} = -\frac{3}{2}\mathbf{H}^n + \frac{1}{2}\mathbf{H}^{n-1} + \frac{1}{2\operatorname{Re}}(\nabla^2 \mathbf{V}^{n+1} + \nabla^2 \mathbf{V}^n) - \nabla \mathbf{P}^{n+1}.$$
(12)

The corrector step employs the following scheme

$$\frac{\mathbf{V}^{n+1} - \mathbf{\tilde{V}}}{\Delta t} = \frac{1}{2\operatorname{Re}} (\nabla^2 \mathbf{V}^{n+1} - \nabla^2 \mathbf{V}) - \nabla P^{n+1} =: -\nabla \varphi^{n+1},$$
(13)

where it is obtained by the subtraction (11) from (12). Taking the divergence of (13) results in

$$\frac{\nabla \cdot \mathbf{V}^{n+1} - \nabla \cdot \hat{\mathbf{V}}}{\Delta t} = -\nabla^2 \varphi^{n+1}.$$
(14)

Now, enforcing continuity at the time level (n+1),

$$\nabla \cdot \mathbf{V}^{n+1} = \mathbf{0},\tag{15}$$

we have from (14):

$$\frac{\nabla \cdot \hat{\mathbf{V}}}{\Delta t} = \nabla^2 \varphi^{n+1}.$$
(16)

The solution process can now be constructed as follows.

Step 1. Solve for V from (11):

$$\frac{\hat{\mathbf{V}}}{\Delta t} - \frac{1}{2\operatorname{Re}} \nabla^2 \hat{\mathbf{V}} = -\frac{3}{2} \mathbf{H}^n + \frac{1}{2} \mathbf{H}^{n-1} + \frac{1}{2\operatorname{Re}} \nabla^2 \mathbf{V}^n + \frac{\mathbf{V}^n}{\Delta t} \,. \tag{17}$$

Multiplying through by Δt , the x component of (17) can be written in Cartesian coordinates:

$$\hat{u}_{i,j} - \frac{\Delta t}{2\operatorname{Re}} \nabla^2 \hat{u}_{i,j} = -\frac{3\Delta t}{2} (H_u^n)_{i,j} + \frac{\Delta t}{2} (H_u^{n-1})_{i,j} + \frac{\Delta t}{2\operatorname{Re}} \nabla^2 u_{i,j}^n + u_{i,j}^n .$$
(18)

Using second-order central difference approximations with $\Delta x = \Delta y = h$, we obtain

$$-\hat{u}_{i+1,j} - \hat{u}_{i,j+1} - \hat{u}_{i,j+1} - \hat{u}_{i,j-1} + (4 + \beta_1)\hat{u}_{i,j} = (RHS_u^n)_{i,j} .$$
⁽¹⁹⁾

The quantities β_1 and (RHS_u^n) are defined respectively as

$$\beta_1^{-1} = \frac{\Delta t}{2 \operatorname{Re} h^2} \,, \tag{20}$$

and

$$(RHS_{u}^{n})_{i,j} = -\frac{3\Delta t\beta_{1}}{2}(H_{u}^{n})_{i,j} + \frac{\Delta t\beta_{1}}{2}(H_{u}^{n-1})_{i,j} + (u_{i+1,j}^{n} - 2u^{n} + u_{i-1,j}^{n}) + (u_{i,j+1}^{n} - 2u_{i,j}^{n} + u_{i,j-1}^{n}) + \beta_{1}u_{i,j}^{n}.$$
(21)

Equation (20) can be rewritten as:

$$-\hat{u}_{i+1,j} - \hat{u}_{i,j+1} - \hat{u}_{i,j+1} - \hat{u}_{i,j-1} + (4 + \beta_1)\hat{u}_{i,j} = (RHS_u^n)_{i,j} .$$
⁽²²⁾

Step 2. Solve for ϕ^{n+1} using (16) with second-order central difference approximations. This equations is written as

$$(\varphi_{i+1,j}^{n+1} + \varphi_{i-1,j}^{n+1} + \varphi_{i,j+1}^{n+1} + \varphi_{i,j-1}^{n+1} - 4\varphi_{i,j}^{n+1}) = \frac{h^2}{\Delta t} \left(\frac{\partial \hat{u}}{\partial x} + \frac{\partial \hat{v}}{\partial y}\right).$$
(23)

Step 3. The velocity field is updated using (13):

$$\frac{\mathbf{V}^{n+1} - \hat{\mathbf{V}}}{\Delta t} = -\nabla \varphi^{n+1},\tag{24}$$

that is,

$$\mathbf{V}^{n+1} = \hat{\mathbf{V}} - (\Delta t) \nabla \varphi^{n+1} .$$
(25)

Writing (25) component-wisely, we have

$$u_{i+1/2,j}^{n+1} = \hat{u}_{i+1/2,j}^n - (\Delta t) \frac{\partial \varphi}{\partial x} \Big|_{i,j}^{n+1}, \qquad (26)$$

and

$$v_{i,j+1/2}^{n+1} = \hat{v}_{i+1/2,j}^n - (\Delta t) \frac{\partial \varphi}{\partial y} \Big|_{i,j}^{n+1}.$$
(27)

Note that in Step 3 above, the variables $\hat{u}_{i+1/2,j}^n$ and $\hat{v}_{i+1/2,j}^n$ are defined at staggered grids and obtained from the following procedure. First we take into account that the following derivative approximations are used in the computations:

$$\left(\frac{\partial u}{\partial t}\right)_{i+1/2,i}^{n+1} = \frac{(u_{i+1/2,j}^{n+1} - u_{i+1/2,j}^{n})}{\Delta t},$$
(28)

$$\left(\frac{\partial^2 u}{\partial x^2}\right)_{i+1/2,j}^{n+1} = \frac{\left(u_{i-1/2,j}^{n+1} - 2u_{i+1/2,j}^{n+1} + u_{i+3/2,j}^{n+1}\right)}{\Delta x^2},$$
(29)

$$\left(\frac{\partial P}{\partial x}\right)_{i+1/2,j}^{n+1} = \frac{(P_{i+1,j}^{n+1} - P_{i,j}^{n+1})}{\Delta x}.$$
(30)

Using the Marker-And-Cell method [2], the other terms in equations (9) and (10) are written as

$$\left(\frac{\partial u^2}{\partial x}\right)_{i+1/2,j}^n = \frac{(u_{i+1,j}^2 - u_{i,j}^2)^n}{\Delta x},$$
(31)

$$u_{i+1,j} = \frac{1}{2} (u_{i+1/2,j} + u_{i+3/2,j}), \qquad (32)$$

$$\left(\frac{\partial uv}{\partial y}\right)_{i+1/2,j} = \frac{\left[(uv)_{i+1/2,j+1/2} - (uv)_{i+1/2,j-1/2}\right]}{\Delta y}$$
(33)

$$= \frac{1}{\Delta y} \Big[(u_{i+1/2,j+1/2})(v_{i+1/2,j+1/2}) - (u_{i+1/2,j-1/2})(v_{i+1/2,j-1/2}) \Big],$$

where

$$u_{i+1/2,j+1/2} = \frac{1}{2} (u_{i+1/2,j} + u_{i+1/2,j+1}), \qquad (34)$$

$$v_{i+1/2,j+1/2} = \frac{1}{2} (v_{i+1/2,j} + v_{i+1/2,j+1}), \qquad (35)$$

$$u_{i+1/2,j-1/2} = \frac{1}{2} (u_{i+1/2,j-1} + u_{i+1/2,j}), \qquad (36)$$

$$v_{i+1/2,j-1/2} = \frac{1}{2} (v_{i,j-1/2} + v_{i+1,j-1/2}).$$
(37)

Then we have

$$\frac{\hat{u}_{i+1/2,j} - u_{i+1/2,j}^n}{\Delta t} = \frac{(u_{i,j}^n)^2 - (u_{i+1,j}^n)^2}{\Delta x} + \frac{(uv)_{i+1/2,j-1/2}^n - (uv)_{i+1/2,j+1/2}^n}{\Delta y} + \frac{1}{\operatorname{Re}\Delta x^2} (u_{i+3/2,j}^n - 2u_{i+1/2,j}^n + u_{i-1/2,j}^n) + \frac{1}{\operatorname{Re}\Delta y^2} (u_{i+1/2,j}^n - 2u_{i+1/2,j}^n + u_{i+1/2,j-1}^n),$$
(38)

and

$$\frac{\hat{v}_{i,j+1/2} - v_{i,j+1/2}^n}{\Delta t} = \frac{(uv)_{i-1/2,j+1/2}^n - (uv)_{i+1/2,j+1/2}^n}{\Delta x} + \frac{(v_{i,j}^n)^2 - (v_{i,j+1}^n)^2}{\Delta y} + \frac{1}{\operatorname{Re}\Delta x^2} (v_{i+1,j+1/2}^n - 2v_{i,j+1/2}^n + v_{i-1,j+1/2}^n) + \frac{1}{\operatorname{Re}\Delta y^2} (v_{i,j+3/2}^n - 2v_{i,j+1/2}^n + v_{i,j-1/2}^n).$$
(39)

The necessary conditions for stability of the method are:

$$c_1(t) \coloneqq \max_{i,j} \left[\Delta t \left(\frac{|u_{i,j}|}{\Delta x_i} + \frac{|v_{i,j}|}{\Delta y_j} \right) \right] \prec 0.5 , \qquad (40)$$

and

$$c_2(t) = \max_{i,j} \left[\frac{\Delta t}{\operatorname{Re}} \left(\frac{1}{\left(\Delta x_i \right)^2} + \frac{1}{\left(\Delta y_j \right)^2} \right) \right] \prec 0.1,$$
(41)

where the notation " \prec " means "less than about."

4 NUMERICAL RESULTS

In this section we present the simulation results of the staggered grid finite difference method. We consider the lid-driven cavity flow problem, where the space domain in a unit square, that is, all points $(x,y) \in [0,1] \times [0,1]$. The initial condition in the unit square is fluid at rest. The boundary conditions are solid wall, except the positions (x, 1) with all $x \in [0, 1]$ having velocity u(x, t) = 1 and v(x, t) = 0. This test is taken from the work of Biringen and Chow [1], Huser and Biringen [3], Li [4] and Erturk et al. [5].



Figure 1. Streamlines for mesh size $99\!\times\!99$.

Taking the viscosity $\mu = 1000$, we obtain the streamlines at the steady state as shown in Figure 1. Here we use the mesh size 99×99 . The results are similar to those of Li [4] and Erturk et al. [5], which means that our numerical solutions are correct up to a tolerance. Here we have used the tolerance is 10^{-9} for the difference between the maximum of absolute velocities u^n at time t^n and u^{n+1} at time t^{n+1} . We note that this tolerance may not be very strict, because the machine precision is 10^{-15} . However we are confident with this solution as it has the correct behaviour. The solution produces three clear vortices: one at the center, one at the bottom left corner and another one at the bottom right corner of the space domain.

When we plot the velocity profile and compare with the available benchmark data (see the data of Erturk et al. [5]), we find that our numerical solutions mimic the benchmark data. The benchmark data is obtained from a different numerical method, and the data is not an analytical solution. Even though some errors occur, but these errors are not very large, as illustrated in Figure 2 and Figure 3. The errors could be reduced if we used smaller tolerance. In addition, the errors are compromised with the simplicity of the numerical method we have used here.



Figure 2. Horizontal profile of velocity field u at x=0,5 for mesh size 99×99 . Here the horizontal axis is the velocity u in the x-direction. The vertical axis is the y-positions corresponding to x=0,5. The solid line is the present solution. The dashed line is the benchmark data of Erturk et al. [5].



Figure 3. Vertical profile of velocity field y at y=0,5 for mesh size 99×99 . Here the horizontal axis is the variable y. in the y-direction. The vertical axis is the x-positions corresponding to y=0,5. The solid line is the present solution. The dashed line is the benchmark data of Erturk et al. [5].

5 CONCLUSION

The staggered grid finite difference method has been tested to solve the lid-driven cavity flow problem. We find that the method is simple to implement, and it couples the velocity and the pressure of the fluid resulting in a stable solution. The solution is relatively accurate with respect to available benchmark data. In general the method is robust, and may be used to solve problems with high Reynold numbers, which could be our future research.

6 REFERENCES

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